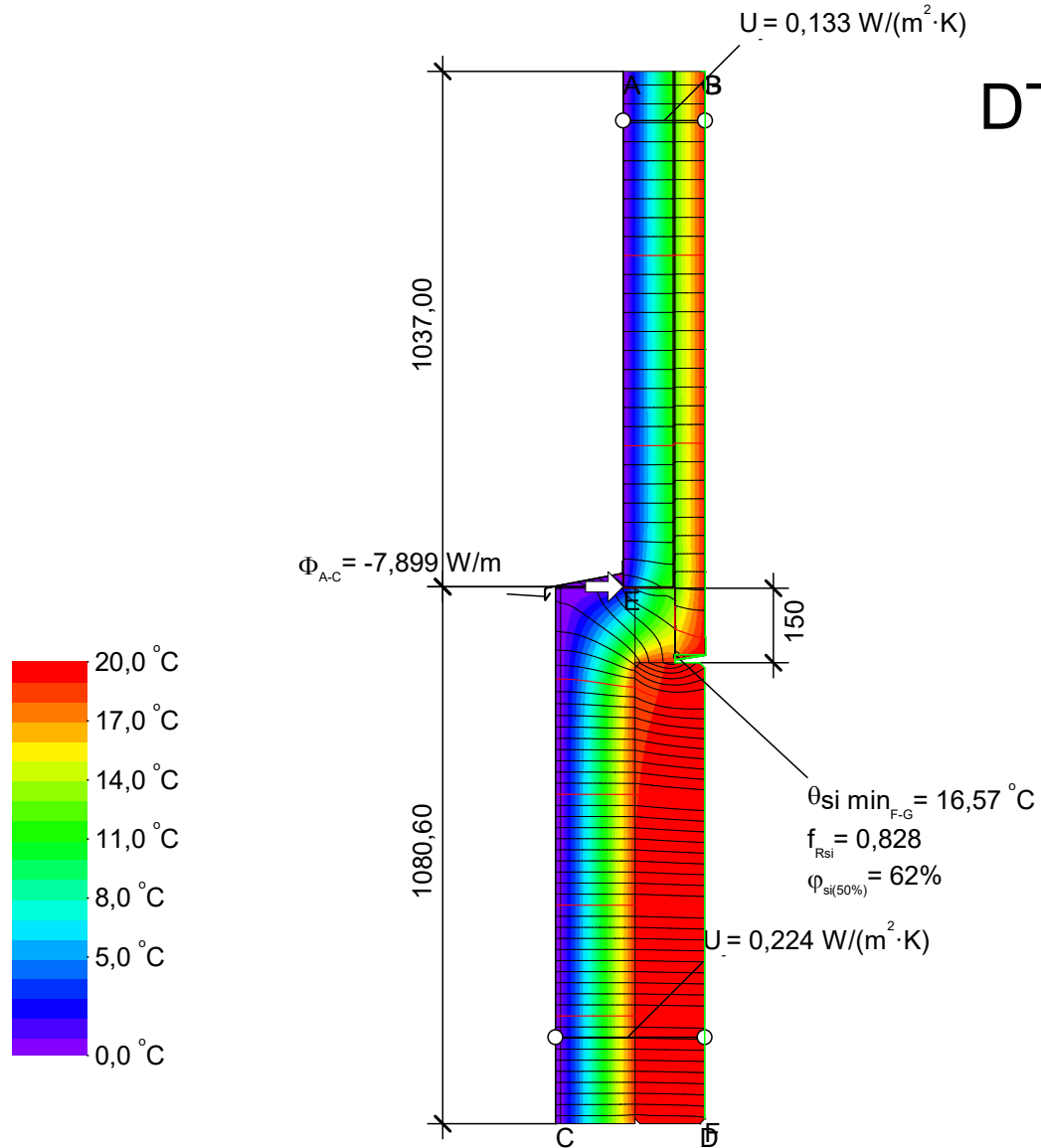


DT 2A.1.1



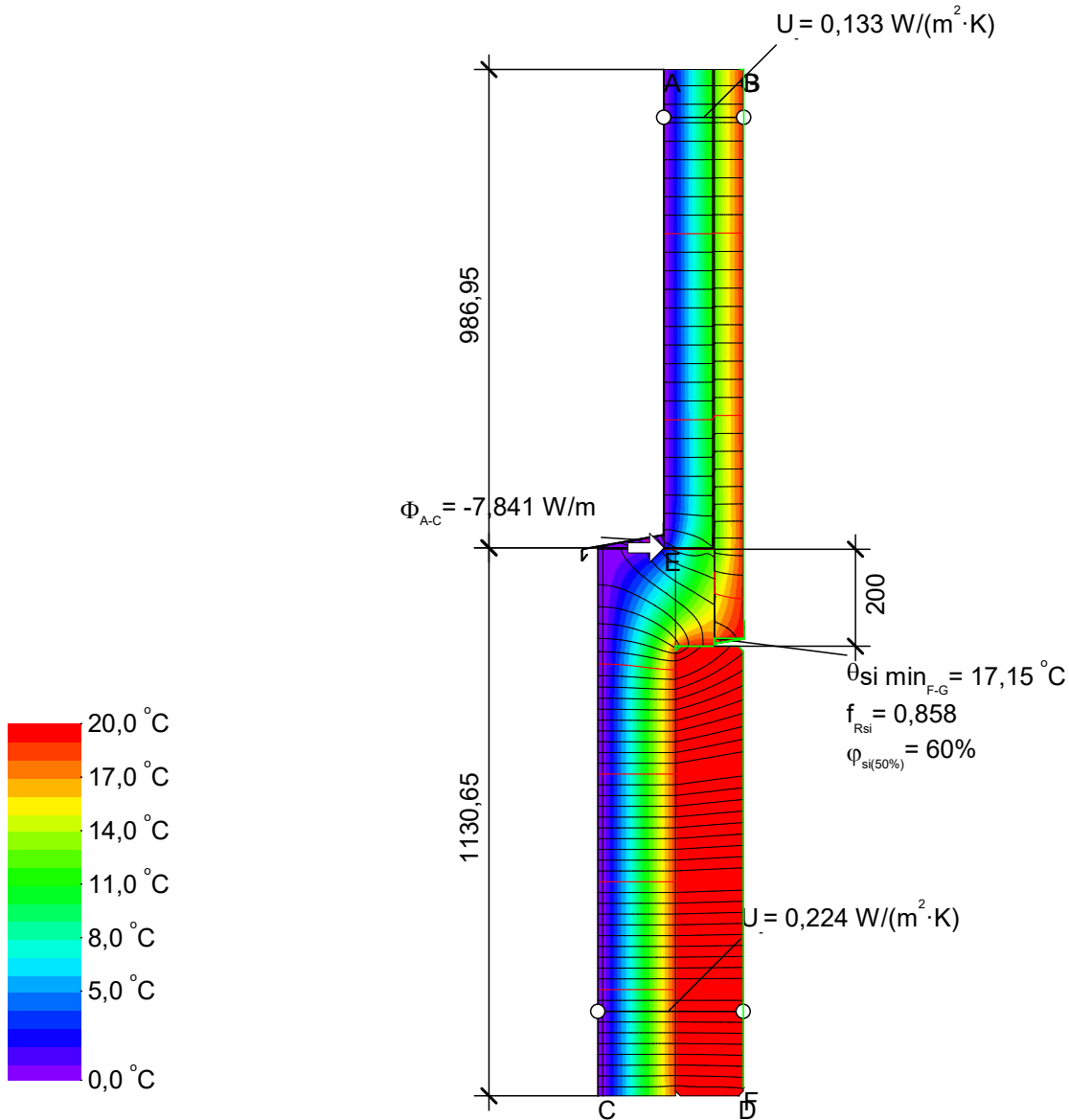
$$\Psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{7,899}{20,000} - 0,133 \cdot 1,037 - 0,224 \cdot 1,081 = 0,015 \text{ W}/(\text{m} \cdot \text{K})$$

Material	λ [W/(m·K)]	ϵ
Concrete, medium density 2200 kg/m ³	1,650	0,900
Foamglas® - 0,036W/mK - Type T3+	0,036	0,900
PIR	0,021	0,900
Slightly ventilated air cavity **		
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	0,900
Unventilated air cavity **		
rotswol	0,032	0,900
sandwichp PUR	0,023	0,900
trespa	0,300	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m ²]	θ [°C]	R [(m ² ·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal		0,000	0,040	
Interior, normal, horizontal		20,000	0,130	
Symmetry/Model section	0,000			

DT 2A.1.2



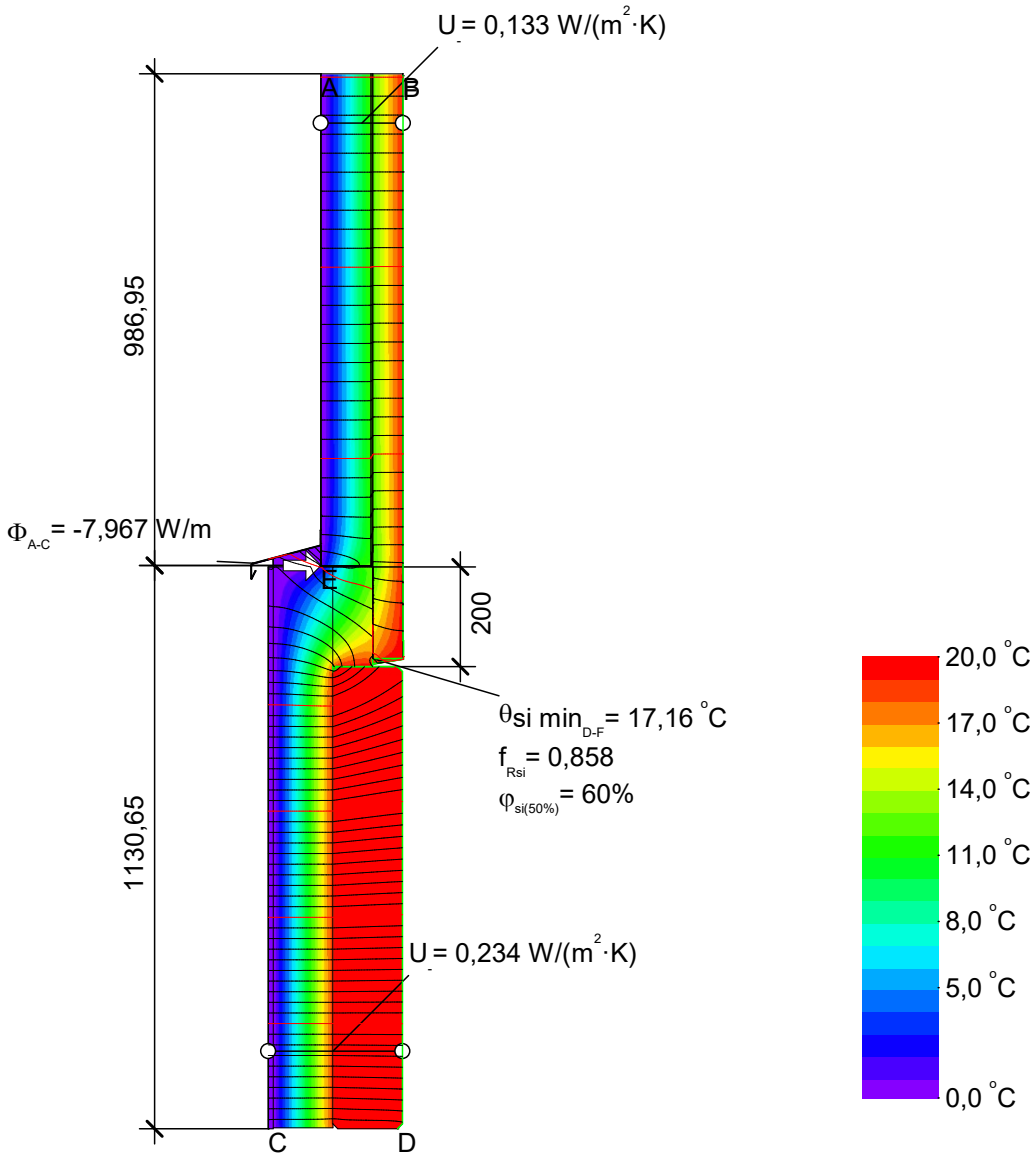
$$\psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{7,841}{20,000} - 0,133 \cdot 0,987 - 0,224 \cdot 1,131 = 0,007 \text{ W/(m} \cdot \text{K)}$$

Material	λ [W/(m·K)]	ϵ
Concrete, medium density 2200 kg/m ³	1,650	0,900
Foamglas® - 0,036W/mK - Type T3+	0,036	0,900
PIR	0,021	0,900
Slightly ventilated air cavity **		
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	0,900
Unventilated air cavity **		
rotswol	0,032	0,900
sandwichp PUR	0,023	0,900
trespa	0,300	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m ²]	θ [°C]	R [(m ² ·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal	0,000		0,040	
Interior, normal, horizontal	20,000		0,130	
Symmetry/Model section	0,000			

DT 2A.1.3



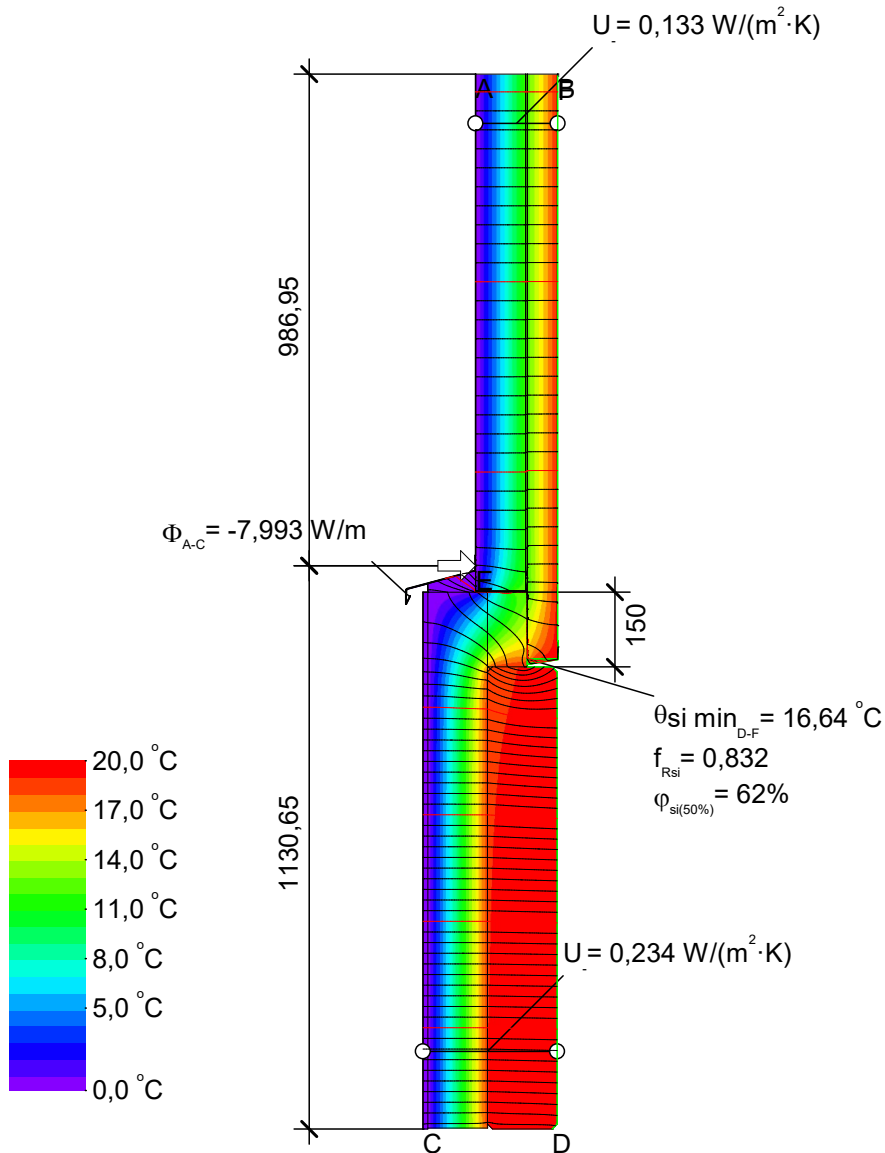
$$\psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{7,967}{20,000} - 0,133 \cdot 0,987 - 0,234 \cdot 1,131 = 0,003 \text{ W}/(\text{m} \cdot \text{K})$$

Material	λ [W/(m·K)]	ϵ
Concrete, medium density 2200 kg/m3	1,650	0,900
PIR	0,021	0,900
Slightly ventilated air cavity **		
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	0,900
Unventilated air cavity **		
XPS	0,030	0,900
rotswol	0,032	0,900
sandwichp PUR	0,023	0,900
trespa	0,300	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m ²]	θ [°C]	R [(m ² ·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal	0,000		0,040	
Interior, normal, horizontal	20,000		0,130	
Symmetry/Model section	0,000			

DT 2A.1.4



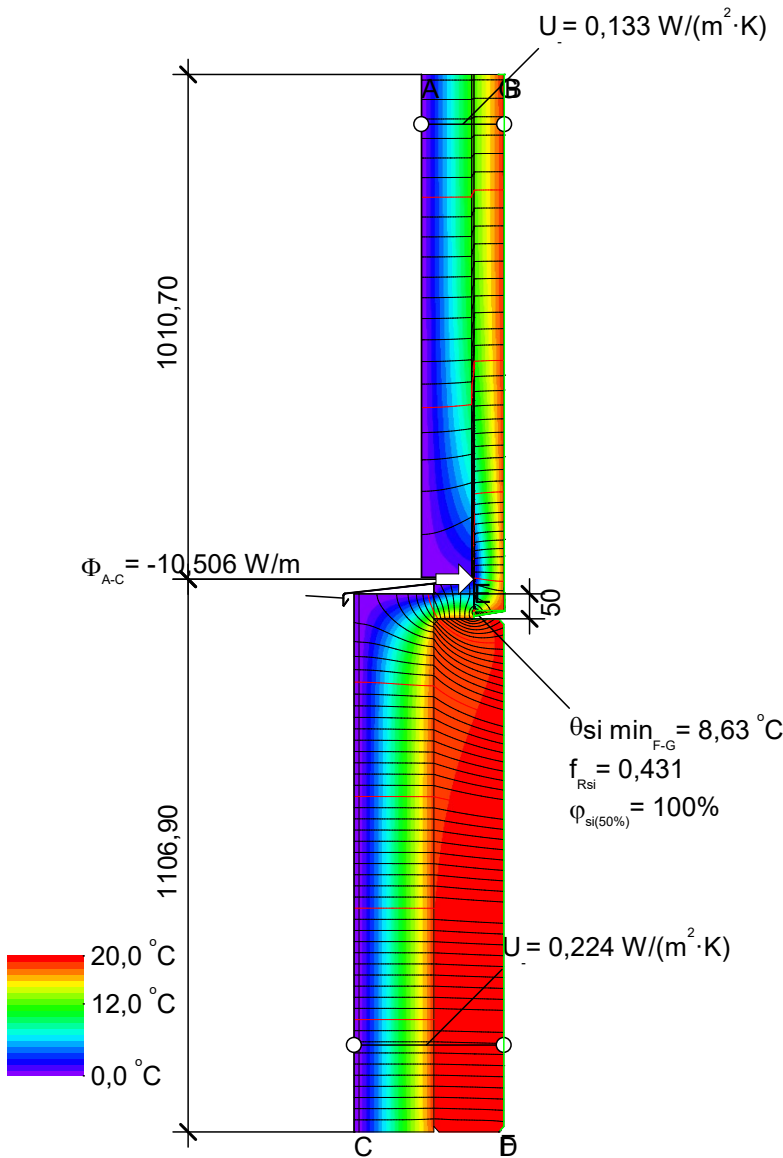
$$\Psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{7,993}{20,000} - 0,133 \cdot 0,987 - 0,234 \cdot 1,131 = 0,004 \text{ W}/(\text{m} \cdot \text{K})$$

Material	λ [W/(m·K)]	ϵ
Concrete, medium density 2200 kg/m3	1,650	0,900
PIR	0,021	0,900
Slightly ventilated air cavity **		
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	0,900
Unventilated air cavity **		
XPS	0,030	0,900
rotswol	0,032	0,900
sandwichp PUR	0,023	0,900
trespa	0,300	0,900

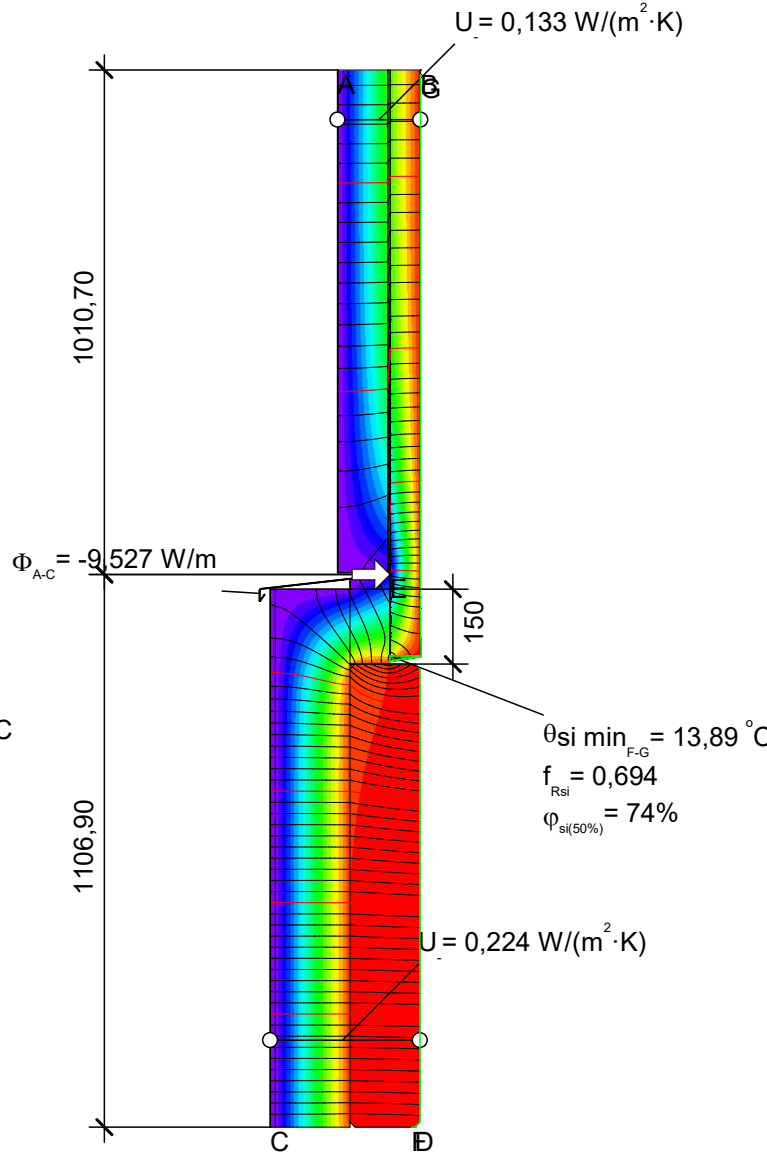
** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m ²]	θ [°C]	R [(m ² ·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal	0,000		0,040	
Interior, normal, horizontal	20,000		0,130	
Symmetry/Model section	0,000			

DT 2A.1.6



DT 2A.1.5



$$\psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{10,506}{20,000} - 0,133 \cdot 1,011 - 0,224 \cdot 1,107 = 0,143 \text{ W}/(\text{m} \cdot \text{K})$$

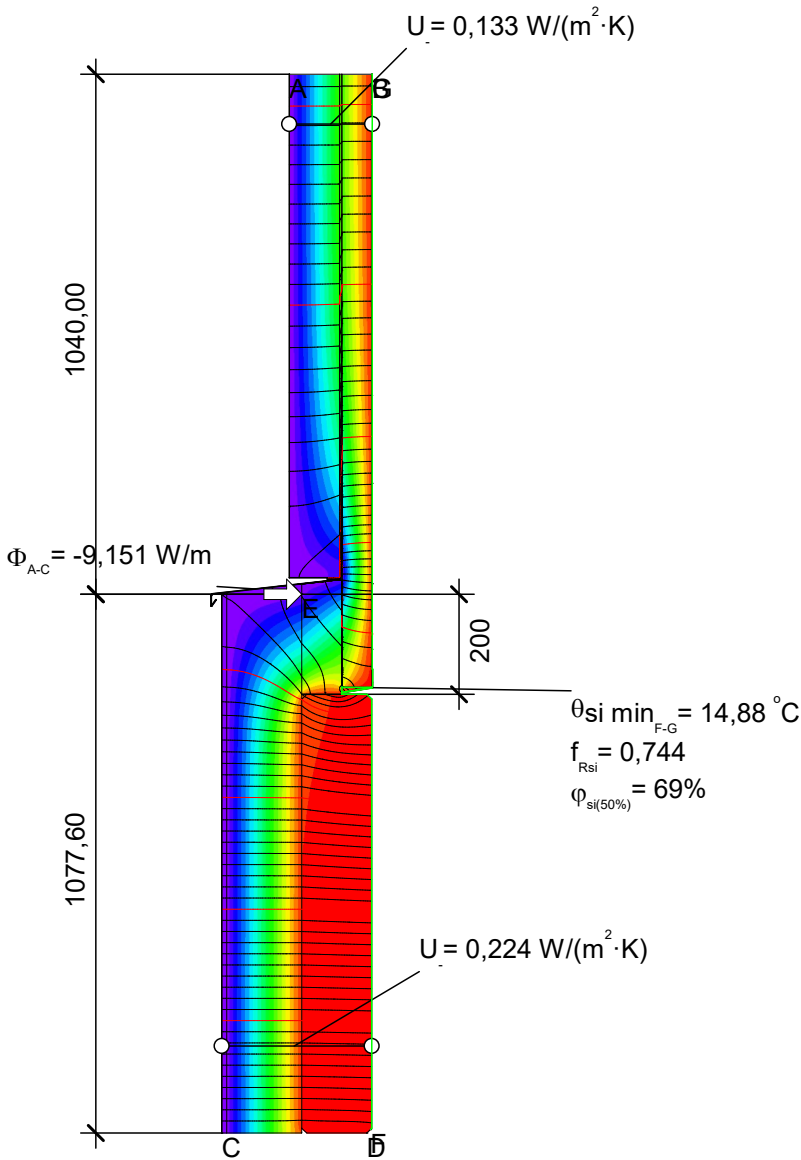
$$\psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{9,527}{20,000} - 0,133 \cdot 1,011 - 0,224 \cdot 1,107 = 0,094 \text{ W}/(\text{m} \cdot \text{K})$$

Material	λ [W/(m·K)]	ϵ
Concrete, medium density 2200 kg/m3	1,650	0,900
Foamglas® - 0,036W/mK - Type T3+	0,036	0,900
PUR sandwich	0,023	0,900
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	0,900
Unventilated air cavity **		
rotswol	0,032	0,900
sandwichpaneel PIR	0,021	0,900
trespa	0,300	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m²]	θ [°C]	R [(m²·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal		0,000	0,040	
Interior, normal, horizontal		20,000	0,130	
Symmetry/Model section	0,000			

DT 2A.1.7



$$\Psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{9,151}{20,000} - 0,133 \cdot 1,040 - 0,224 \cdot 1,078 = 0,078 \text{ W}/(\text{m} \cdot \text{K})$$

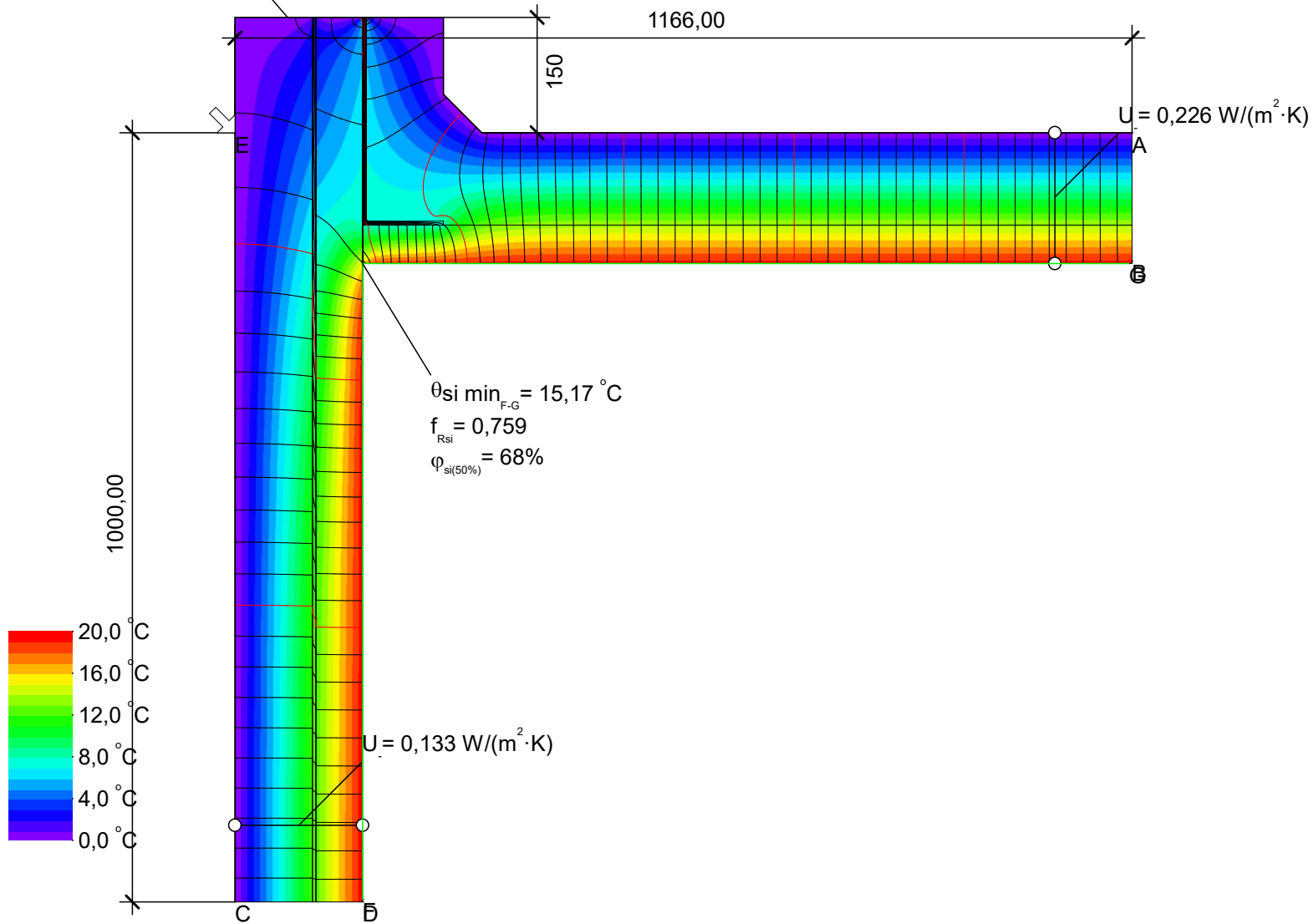
Material	λ [W/(m·K)]	ϵ
Concrete, medium density 2200 kg/m3	1,650	0,900
Foamglas® - 0,036W/mK - Type T3+	0,036	0,900
PUR sandwich	0,023	0,900
Slightly ventilated air cavity **		
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	0,900
Undefined Material	0,010	
Unventilated air cavity **		
isolatie	0,021	0,900
sandwichpaneel PIR	0,021	0,900
trespa	0,300	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m²]	θ [°C]	R [(m²·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal	0,000		0,040	
Interior, normal, horizontal	20,000		0,130	
Symmetry/Model section	0,000			

DT 2A.2.1

$$\Phi_{A-C} = -8,968 \text{ W/m}$$



$$\Psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{8,968}{20,000} - 0,226 \cdot 1,166 - 0,133 \cdot 1,000 = 0,052 \text{ W/(m} \cdot \text{K)}$$

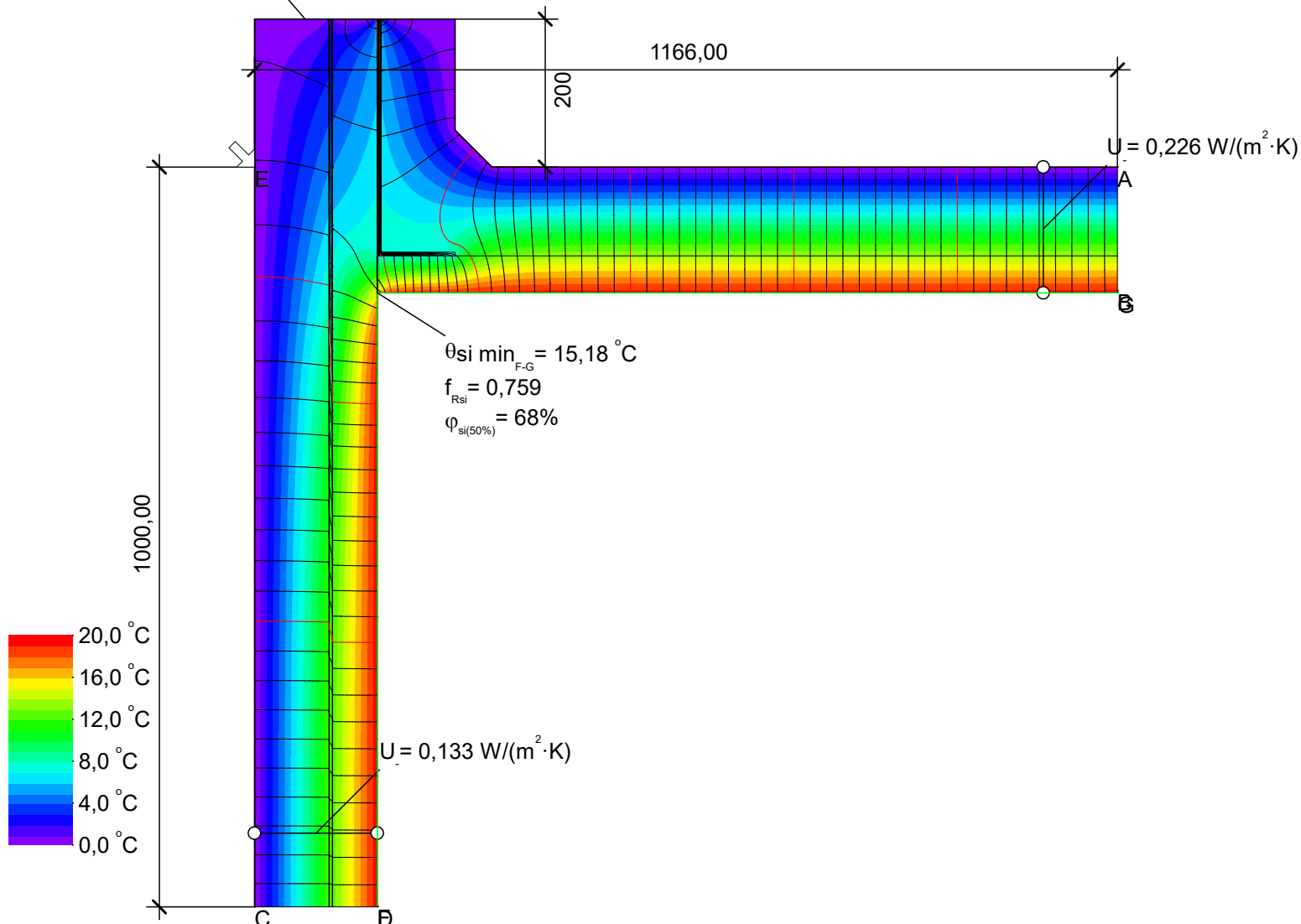
Material	λ [W/(m·K)]	ϵ
PUR sandwich	0,023	0,900
Sandwichpaneel PIR	0,021	0,900
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	
Unventilated air cavity **		
minerale wol	0,040	
rotswol	0,040	

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m ²]	θ [°C]	R [(m ² ·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal		0,000	0,040	
Interior, normal, horizontal		20,000	0,130	
Symmetry/Model section	0,000			

DT 2A.2.2

$\Phi_{A-C} = -8,960 \text{ W/m}$



$$\Psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{8,960}{20,000} - 0,226 \cdot 1,166 - 0,133 \cdot 1,000 = 0,052 \text{ W/(m}\cdot\text{K)}$$

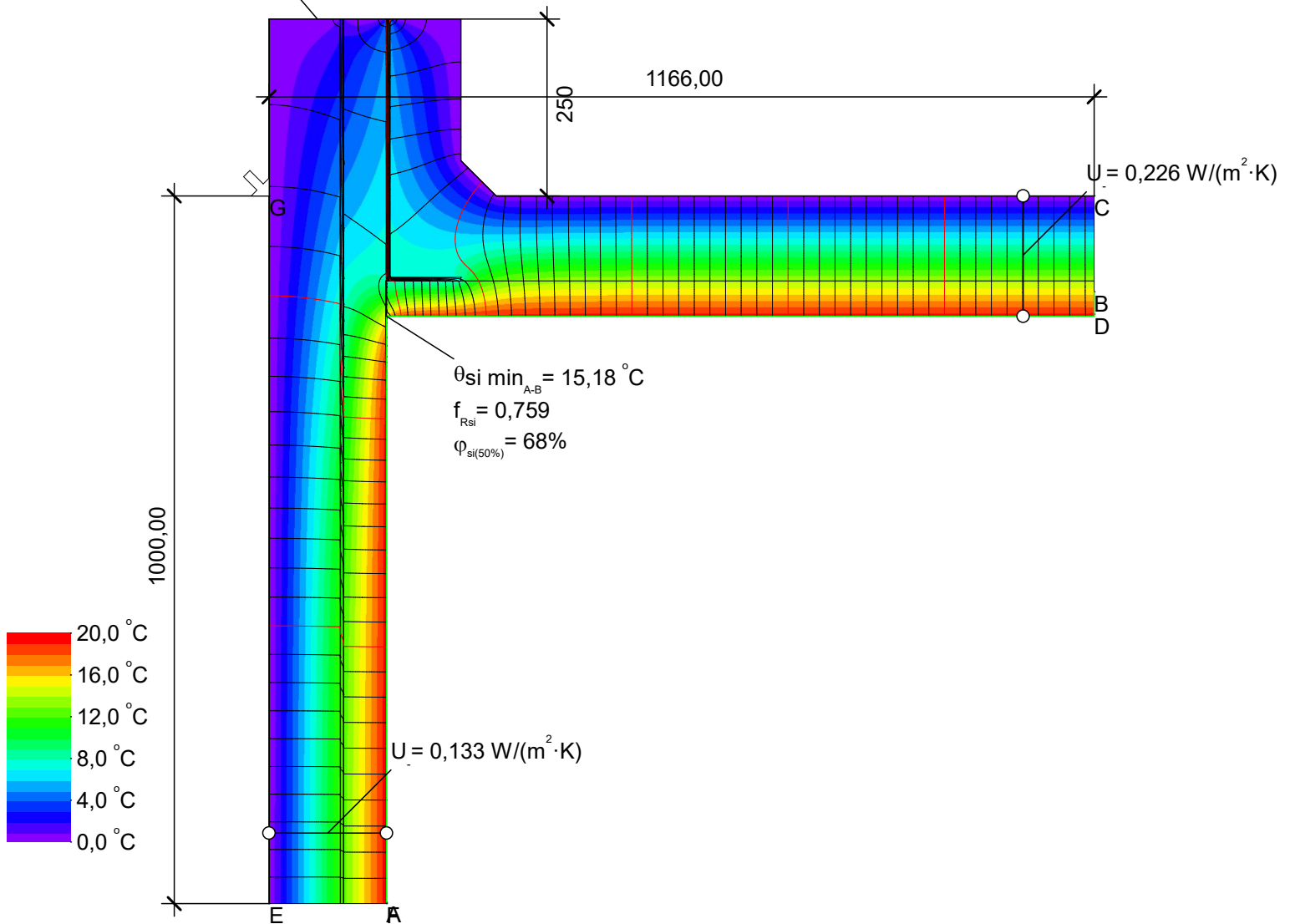
Material	λ [W/(m·K)]	ϵ
PUR sandwich	0,023	0,900
Sandwichpaneel PIR	0,021	0,900
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	
Unventilated air cavity **		
minerale wol	0,040	
rotswol	0,040	

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m²]	θ [°C]	R [(m²·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal		0,000	0,040	
Interior, normal, horizontal		20,000	0,130	
Symmetry/Model section	0,000			

DT 2A.2.3

$\Phi_{C-E} = -8,954 \text{ W/m}$



$$\psi_{C-G-E} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{8,954}{20,000} - 0,226 \cdot 1,166 - 0,133 \cdot 1,000 = 0,051 \text{ W/(m} \cdot \text{K)}$$

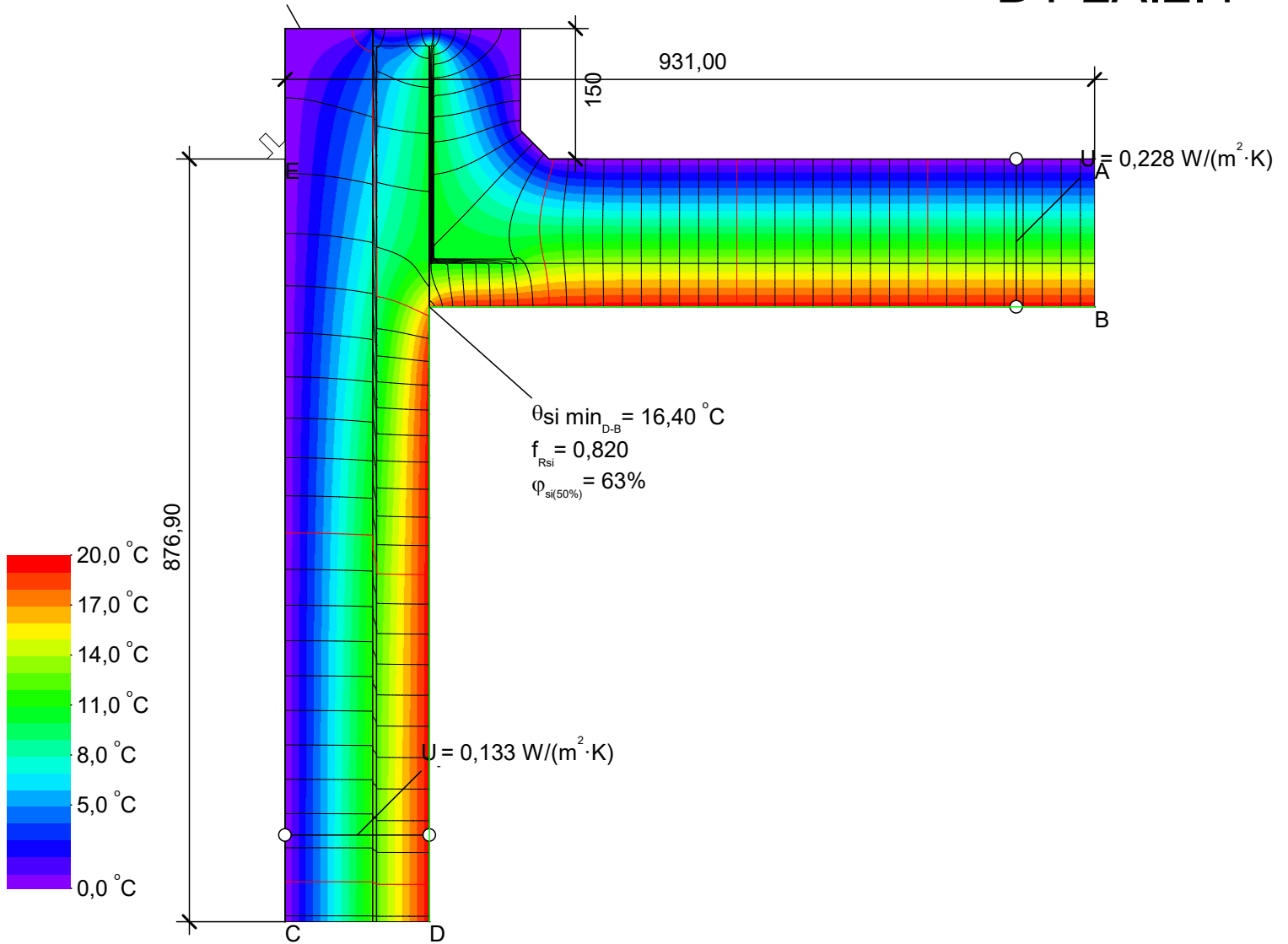
Material	λ [W/(m·K)]	ϵ
PUR sandwich	0,023	0,900
Sandwichpaneel PIR	0,021	0,900
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	
Unventilated air cavity **		
minerale wol	0,040	
rotswol	0,040	

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m²]	θ [°C]	R [(m²·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal		0,000	0,040	
Interior, normal, horizontal		20,000	0,130	
Symmetry/Model section	0,000			

DT 2A.2.4

$\Phi_{A-C} = -6,857 \text{ W/m}$



$\theta_{si \text{ min}_{D-B}} = 16,40 \text{ }^\circ\text{C}$
 $f_{Rsi} = 0,820$
 $\phi_{si(50\%)} = 63\%$

$U = 0,133 \text{ W}/(\text{m}^2 \cdot \text{K})$

$U_A = 0,228 \text{ W}/(\text{m}^2 \cdot \text{K})$

$$\Psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{6,857}{20,000} - 0,228 \cdot 0,931 - 0,133 \cdot 0,877 = 0,014 \text{ W}/(\text{m} \cdot \text{K})$$

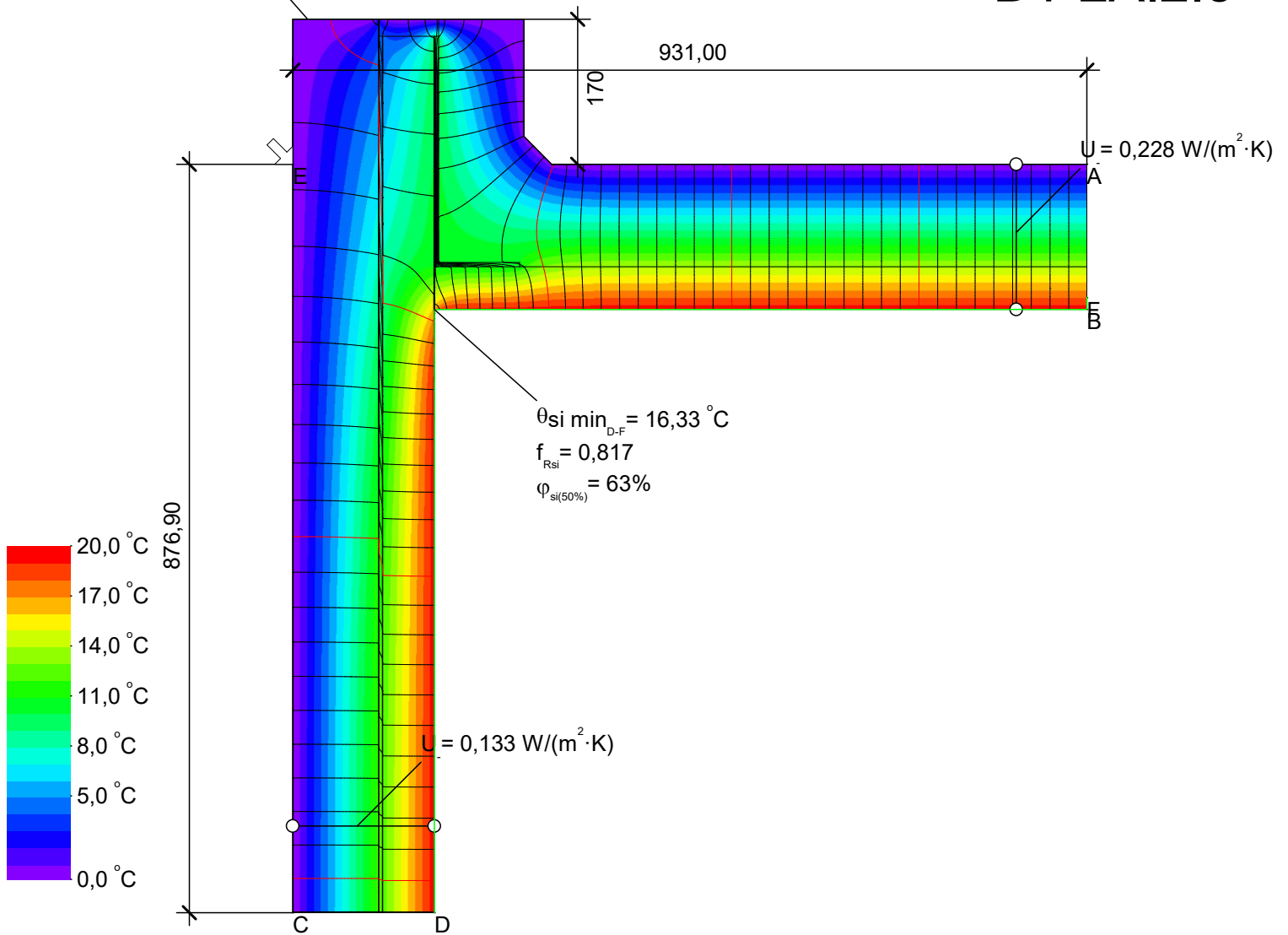
Material	λ [W/(m·K)]	ϵ
PUR sandwich	0,023	0,900
Sandwichpaneel PIR	0,021	0,900
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	
Unventilated air cavity **		
minerale wol	0,040	0,900
rotswol	0,040	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m ²]	θ [°C]	R [(m ² ·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal	0,000		0,040	
Interior, heat flux, upwards	20,000		0,100	
Interior, normal, horizontal	20,000		0,130	
Symmetry/Model section	0,000			

DT 2A.2.5

$\Phi_{A-C} = -6,896 \text{ W/m}$



$$\Psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{6,896}{20,000} - 0,228 \cdot 0,931 - 0,133 \cdot 0,877 = 0,016 \text{ W/(m}\cdot\text{K)}$$

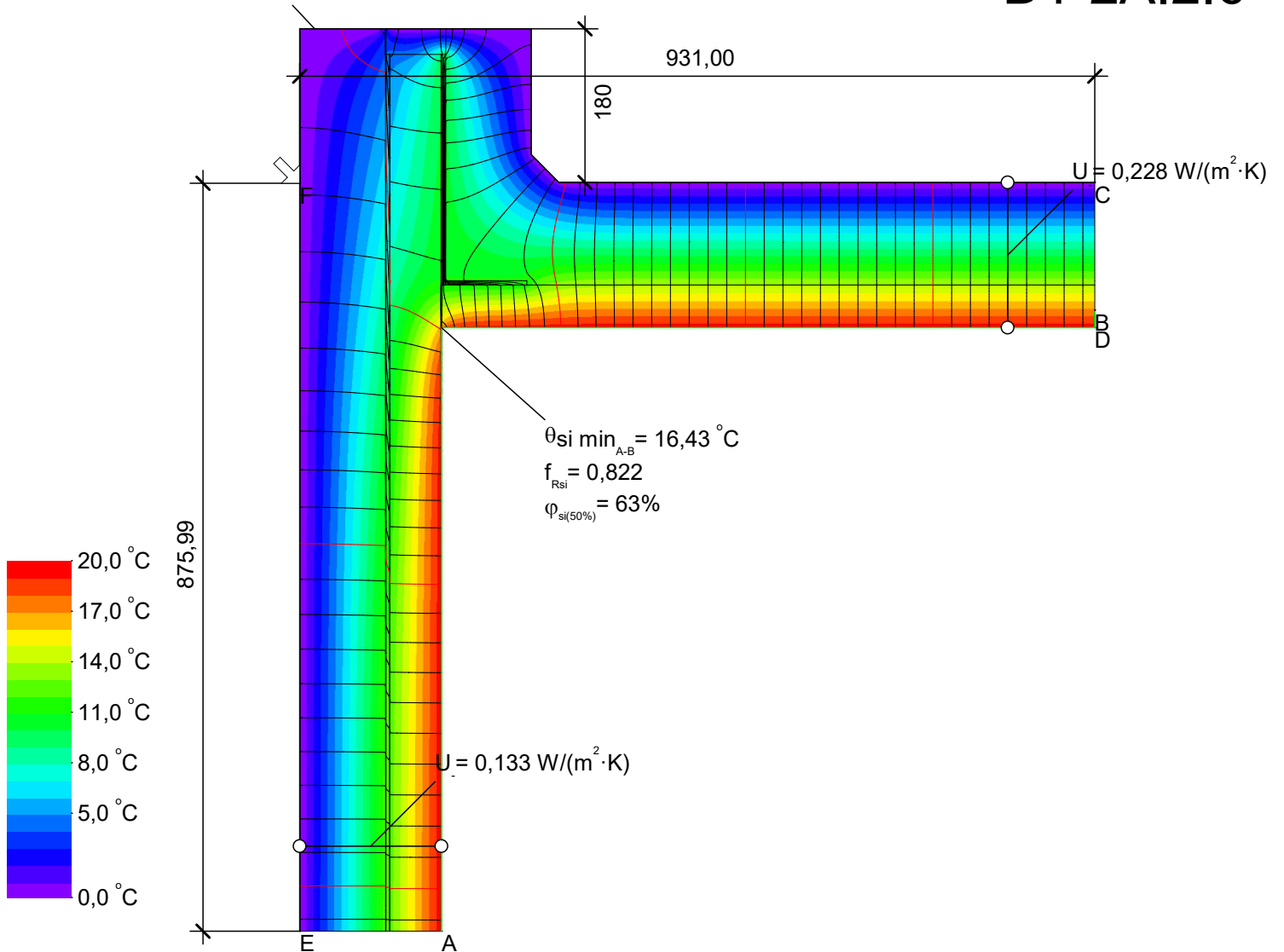
Material	λ [W/(m·K)]	ϵ
PUR sandwich	0,023	0,900
Sandwichpaneel PIR	0,021	0,900
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	
Unventilated air cavity **		
minerale wol	0,040	0,900
rotswol	0,040	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m ²]	θ [°C]	R [(m ² ·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal	0,000		0,040	
Interior, heat flux, upwards	20,000		0,100	
Interior, normal, horizontal	20,000		0,130	
Symmetry/Model section	0,000			

DT 2A.2.6

$\Phi_{C-E} = -6,826 \text{ W/m}$



$$\Psi_{C-F-E} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{6,826}{20,000} - 0,228 \cdot 0,931 - 0,133 \cdot 0,876 = 0,013 \text{ W}/(\text{m} \cdot \text{K})$$

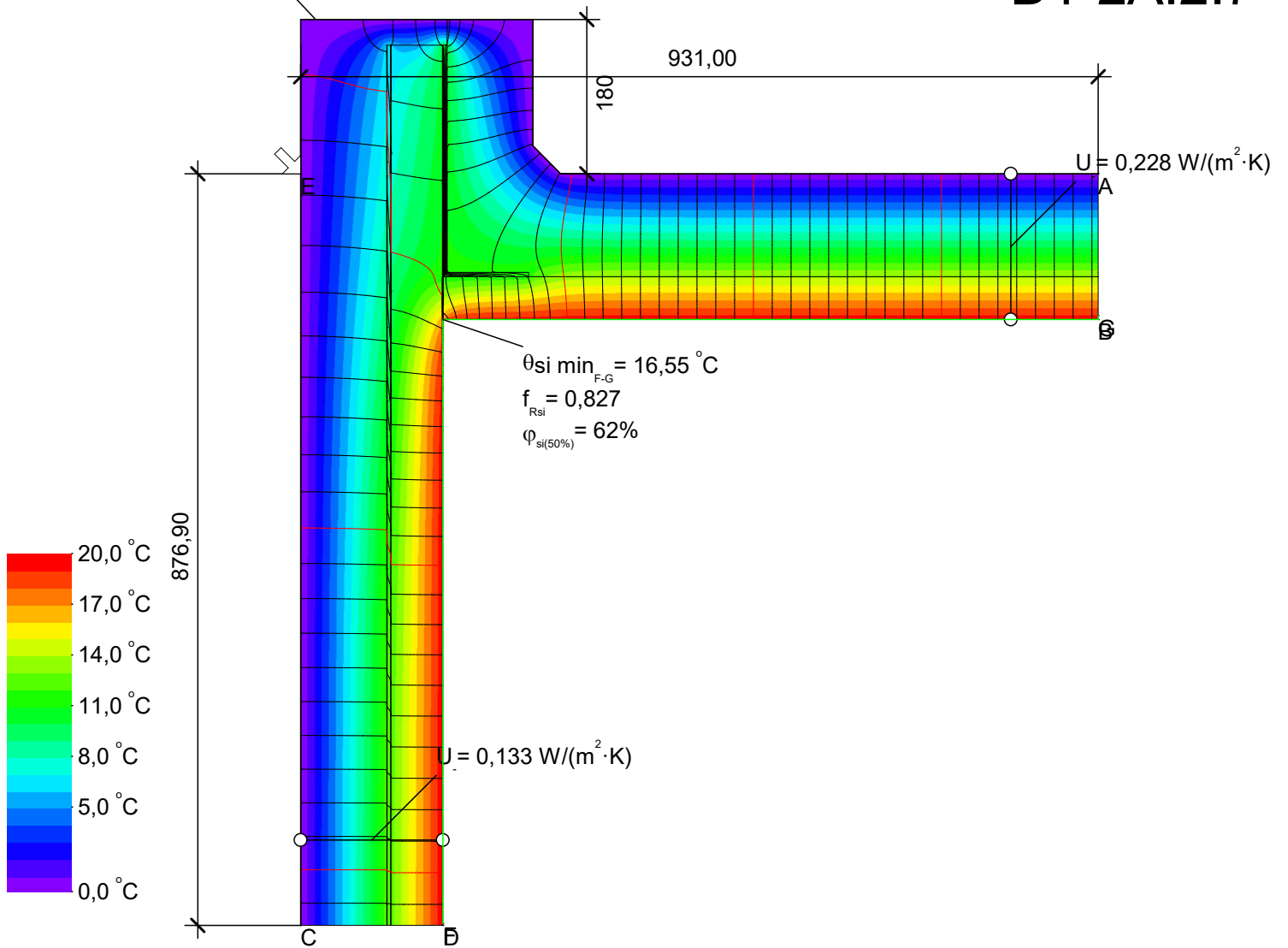
Material	$\lambda[\text{W}/(\text{m} \cdot \text{K})]$	ϵ
PUR sandwich	0,023	0,900
Sandwichpaneel PIR	0,021	0,900
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	
Unventilated air cavity **		
minerale wol	0,040	0,900
rotswol	0,040	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[^\circ\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ϵ
Epsilon 0.9				0,900
Exterior, normal	0,000		0,040	
Interior, heat flux, upwards	20,000		0,100	
Interior, normal, horizontal	20,000		0,130	
Symmetry/Model section	0,000			

DT 2A.2.7

$$\Phi_{A-C} = -6,732 \text{ W/m}$$



$$\Psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{6,732}{20,000} - 0,228 \cdot 0,931 - 0,133 \cdot 0,877 = 0,008 \text{ W}/(\text{m} \cdot \text{K})$$

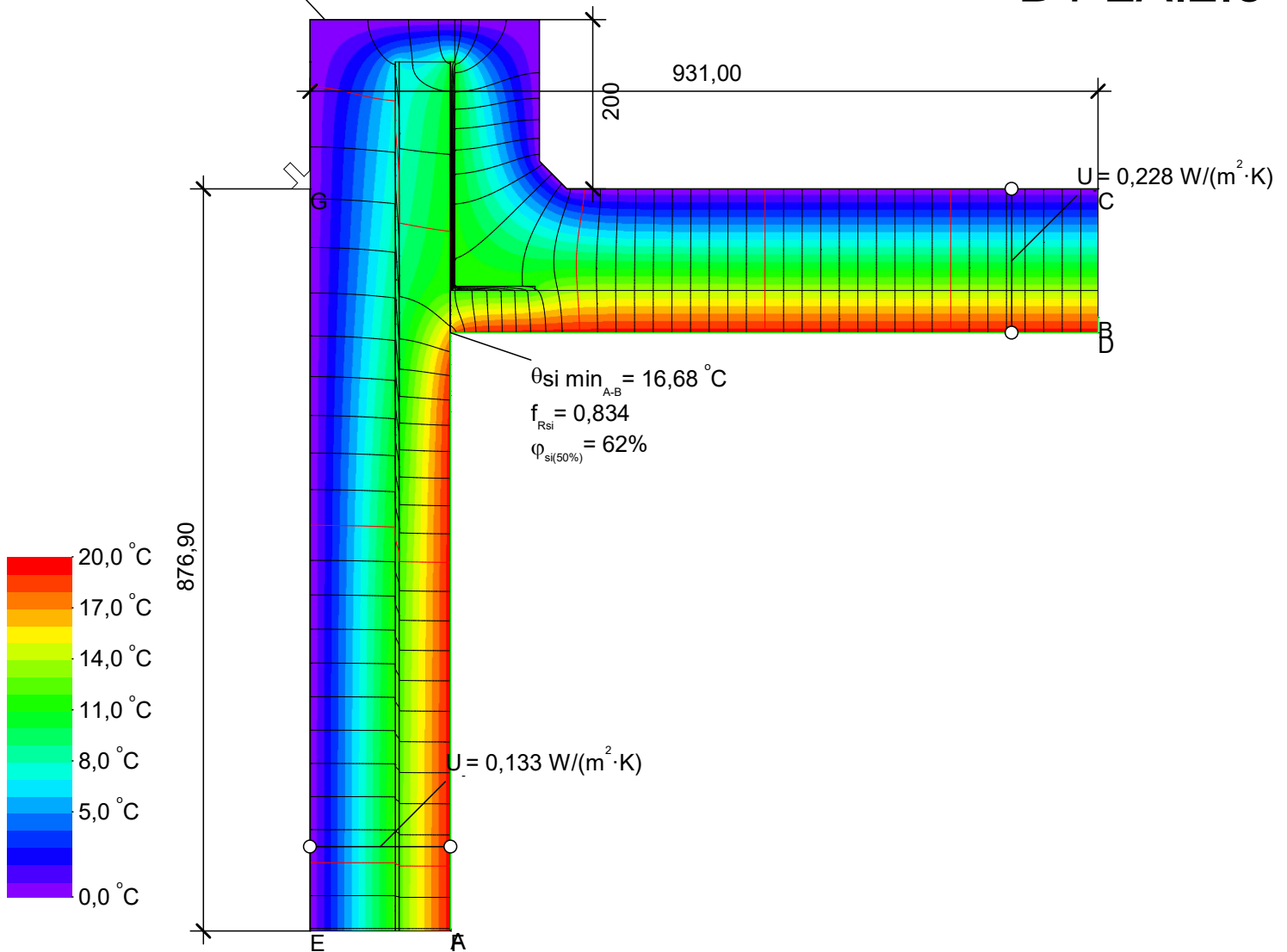
Material	λ [W/(m·K)]	ϵ
PUR sandwich	0,023	0,900
Sandwichpaneel PIR	0,021	0,900
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	
Unventilated air cavity **		
minerale wol	0,040	0,900
rotswol	0,040	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m ²]	θ [°C]	R [(m ² ·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal		0,000	0,040	
Interior, heat flux, upwards	20,000		0,100	
Interior, normal, horizontal		20,000	0,130	
Symmetry/Model section		0,000		

DT 2A.2.8

$$\Phi_{C-E} = -6,641 \text{ W/m}$$



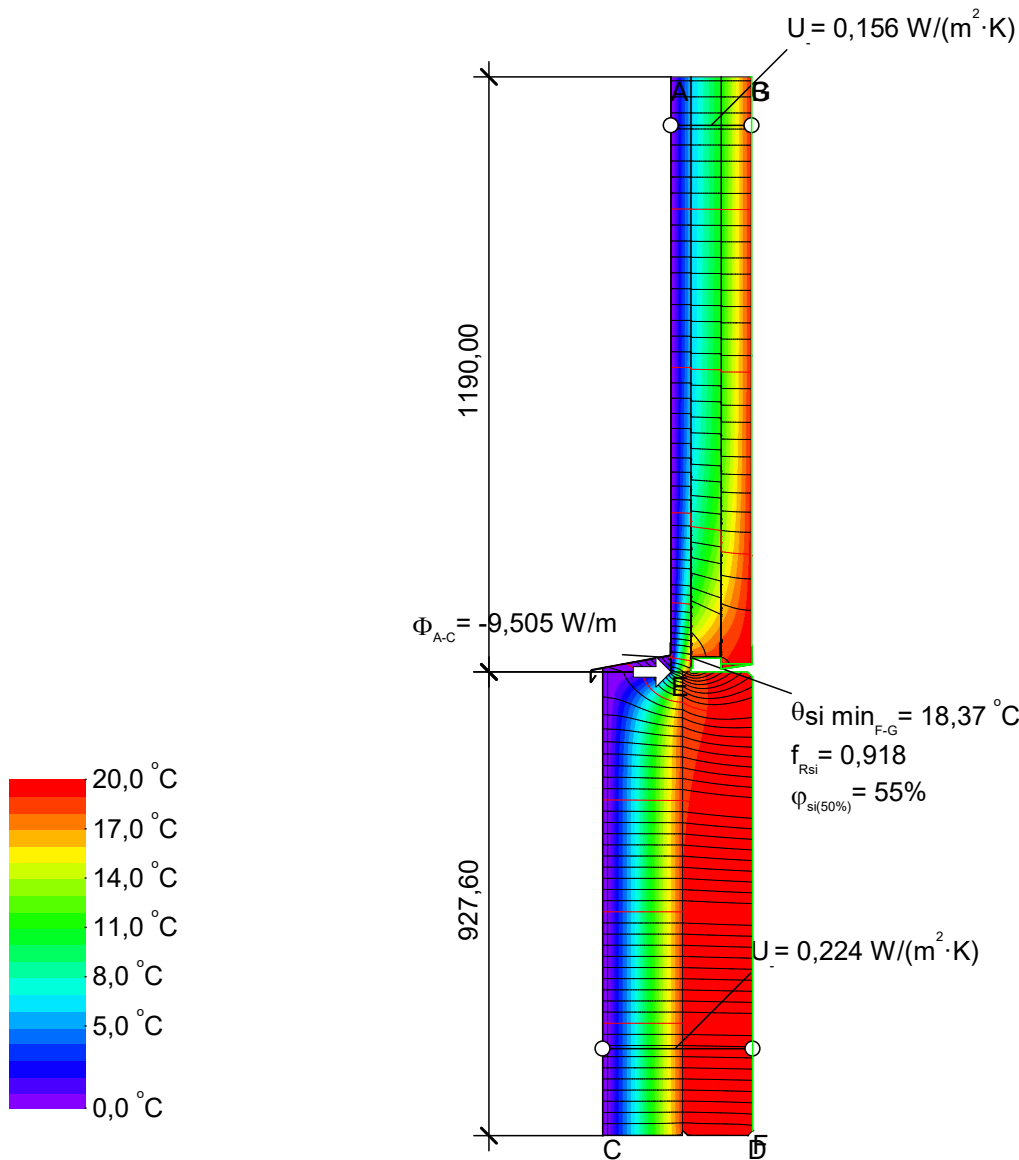
$$\psi_{C-G-E} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{6,641}{20,000} - 0,228 \cdot 0,931 - 0,133 \cdot 0,877 = 0,004 \text{ W/(m} \cdot \text{K)}$$

Material	λ [W/(m·K)]	ϵ
PUR sandwich	0,023	0,900
Sandwichpaneel PIR	0,021	0,900
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	
Unventilated air cavity **		
minerale wol	0,040	0,900
rotswol	0,040	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m²]	θ [°C]	R [(m²·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal		0,000	0,040	
Interior, heat flux, upwards	20,000		0,100	
Interior, normal, horizontal		20,000	0,130	
Symmetry/Model section	0,000			

DT 2B.1.1



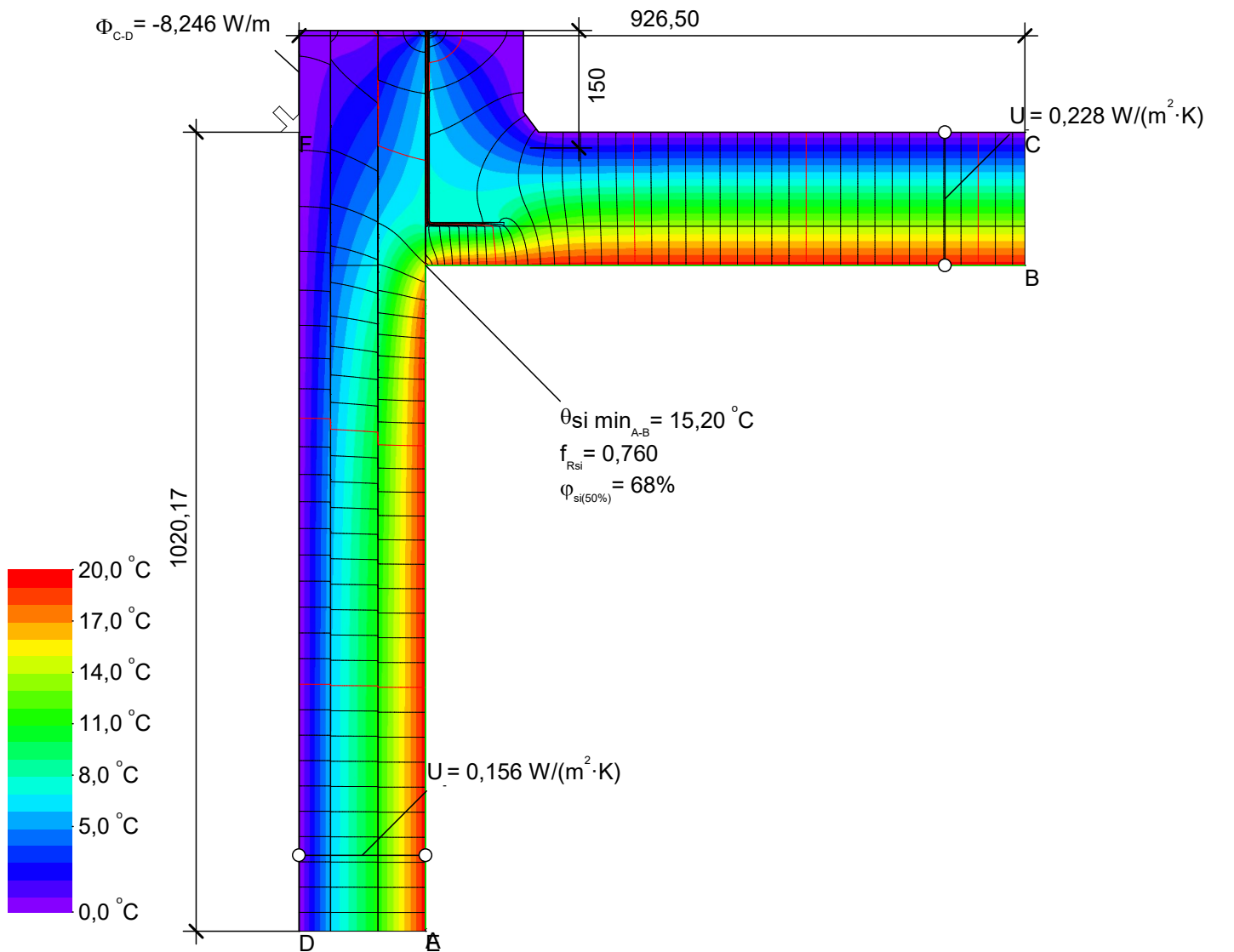
$$\psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{9,505}{20,000} - 0,156 \cdot 1,190 - 0,224 \cdot 0,928 = 0,082 \text{ W}/(\text{m} \cdot \text{K})$$

Material	λ [W/(m·K)]	ϵ
Concrete, medium density 2200 kg/m3	1,650	0,900
Foamglas® - 0,036W/mK - Type T3+	0,036	0,900
PUR sandwich	0,023	0,900
Slightly ventilated air cavity **		
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	0,900
Unventilated air cavity **		
glaswol inblaas	0,034	0,900
sandwich PIR	0,021	0,900
trespa	0,300	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m²]	θ [°C]	R [(m²·K)/W]	ϵ
Epsilon 0.9				0,900
Exterior, normal	0,000		0,040	
Interior, normal, horizontal	20,000		0,130	
Symmetry/Model section	0,000			

DT 2B.2.1

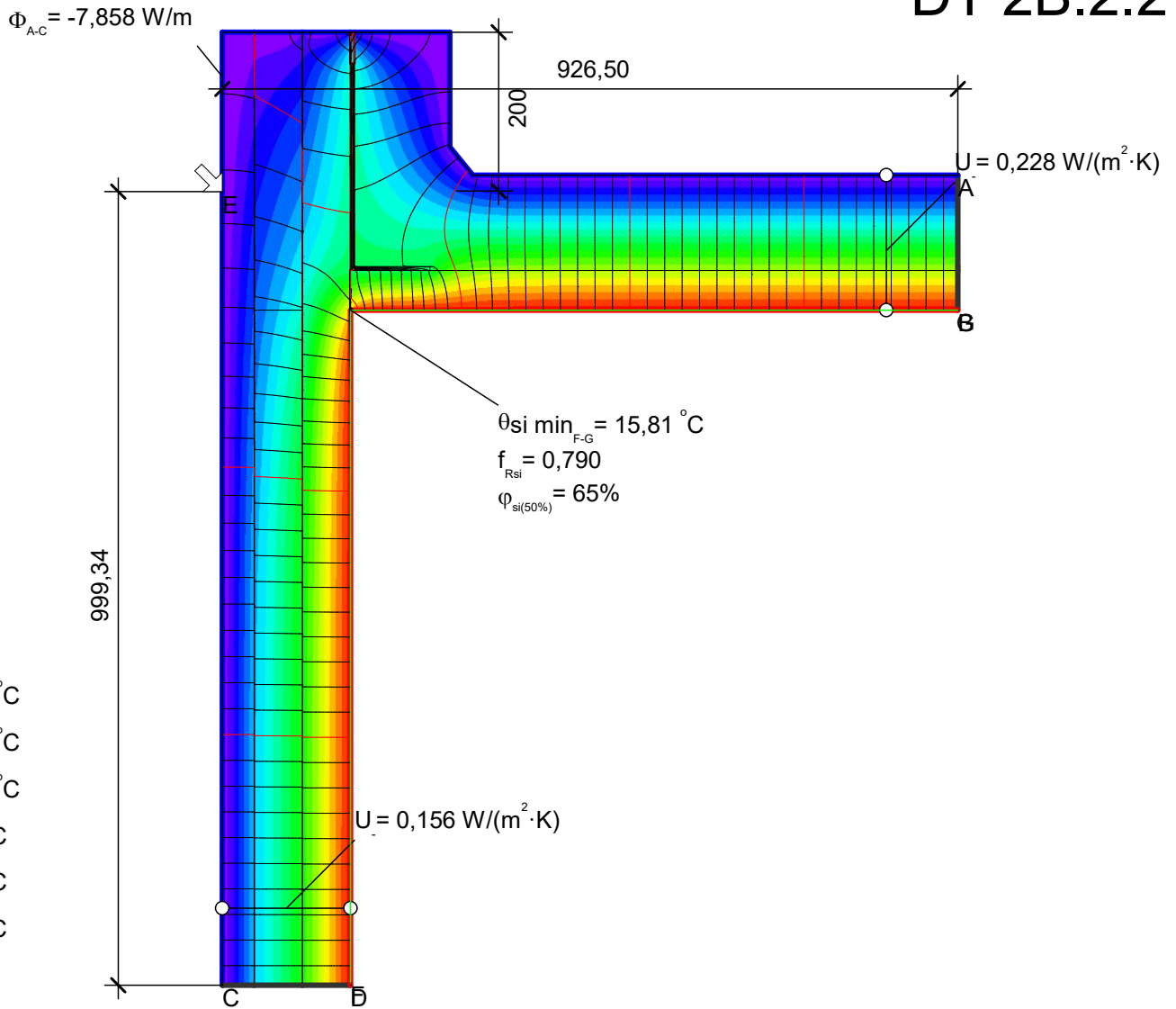


$$\psi_{C-F-D} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{8,246}{20,000} - 0,228 \cdot 0,926 - 0,156 \cdot 1,020 = 0,043 \text{ W}/(\text{m} \cdot \text{K})$$

Material	λ [W/(m·K)]
PUR sandwich	0,023
Sandwichpaneel PIR	0,021
Stainless steel, austenitic or austenitic-ferritic	17,000
Steel	50,000
glaswol inblaas	0,034
minerale wol	0,040
rotswol	0,040

Boundary Condition	q [W/m²]	θ [°C]	R [(m²·K)/W]
Exterior, normal	0,000	0,000	0,040
Interior, heat flux, upwards	20,000	0,000	0,100
Interior, normal, horizontal	0,000	20,000	0,130
Symmetry/Model section	0,000	0,000	0,000

DT 2B.2.2



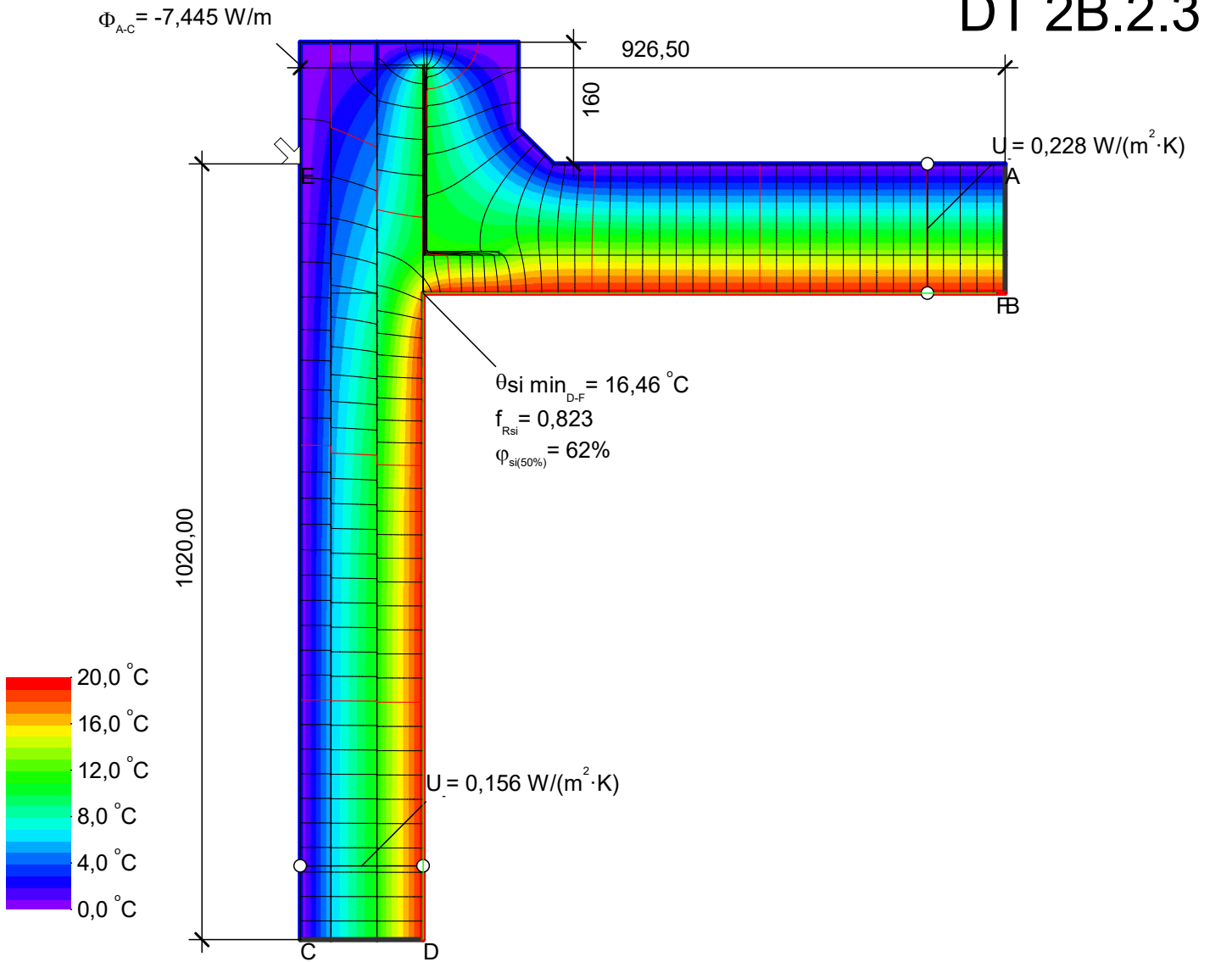
$$\Psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{7,858}{20,000} - 0,228 \cdot 0,927 - 0,156 \cdot 0,999 = 0,026 \text{ W/(m} \cdot \text{K)}$$

Material	λ [W/(m·K)]	ε
PUR sandwich	0,023	0,900
Sandwichpaneel PIR	0,021	0,900
Stainless steel, austenitic or austenitic-ferritic	17,000	0,900
Steel	50,000	0,900
Unventilated air cavity **		
glaswol inblaas	0,034	0,900
minerale wol	0,040	0,900
rotswol	0,040	0,900

** EN ISO 10077-2:2017, 6.4.3/anisotrop

Boundary Condition	q [W/m ²]	θ [°C]	R [(m ² ·K)/W]	ε
Epsilon 0.9				0,900
Exterior, normal		0,000	0,040	
Interior, heat flux, upwards	20,000		0,100	
Interior, normal, horizontal		20,000	0,130	
Symmetry/Model section	0,000			

DT 2B.2.3



$$\Psi_{A-E-C} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{7,445}{20,000} - 0,228 \cdot 0,927 - 0,156 \cdot 1,020 = 0,002 \text{ W/(m}\cdot\text{K)}$$

Material	λ [W/(m·K)]
PUR sandwich	0,023
Sandwichpaneel PIR	0,021
Stainless steel, austenitic or austenitic-ferritic	17,000
Steel	50,000
glaswol inblaas	0,034
minerale wol	0,040
rotswol	0,040

Boundary Condition	q [W/m ²]	θ [°C]	R [(m ² ·K)/W]
Exterior, normal	0,000	0,040	
Interior, heat flux, upwards	20,000	0,100	
Interior, normal, horizontal	20,000	0,130	
Symmetry/Model section	0,000		